

# Generalized Thermoelasticity in Modern Engineering: Trends in Dynamic Multi-Field Modeling

**Dr. Kiran Bala**

Assistant Professor of Mathematics, Government P.G. College for Women, Sector 14, Panchkula

## Abstract

The rapid advancement of high-precision engineering and micro-scale technologies necessitates a transition from classical thermal theories to generalized frameworks that account for finite heat propagation speeds. This review explores the paradigm of Generalized Thermoelasticity within the context of Dynamic Multi-Field Modeling, specifically examining the interplay between rotational dynamics and two-temperature thermal responses. Historically, classical models—grounded in the works of Duhamel and Neumann—suffered from the paradox of infinite heat velocity. Modern components, such as aerospace turbines and high-frequency resonators, operate under extreme rotational speeds and thermal gradients, requiring the hyperbolic models of Lord-Shulman (L-S) and Green-Naghdi (G-N). A central emphasis is placed on the "Two-Temperature" parameter ( $a^*$ ), which distinguishes between conductive and thermodynamic temperatures to accurately predict material behavior under ultra-short thermal loading. Through a comparative analysis of wave speeds and reflection coefficients in high-conductivity media like Copper, this paper identifies critical modeling challenges and trends in energy partitioning at material boundaries. The results demonstrate that incorporating rotational parameters and two-temperature effects is essential for predicting material fatigue and performance in rotating, heat-sensitive engineering systems. This study provides a comprehensive roadmap for the evolution of thermoelasticity from a static theory to a dynamic, multi-field engineering necessity.

**Keywords:** Generalized thermoelasticity, Modelling, Engineering Systems

## 1. Introduction

The foundation of classical thermoelasticity was established in the mid-19th century by Duhamel (1838) and Neumann (1841), who initially formulated equations for strain in elastic bodies subjected to temperature gradients. Early iterations of the theory were limited by the assumption of independence between thermal and mechanical effects, where total strain was determined by simply superimposing elastic strain onto thermal expansion caused by a known temperature distribution. This uncoupled approach failed to account for the interaction between strain and temperature distributions or the motion associated with a material's thermal state. It was not until Thomson (1857) utilized the laws of thermodynamics that the first true integration of mechanical work and heat exchange was achieved, predicting the thermomechanical behavior of elastic solids. Despite these advancements, classical uncoupled and coupled theories—such as those developed by Biot (1956) and Nowacki (1966)—maintained an inherent physical paradox: the assumption that thermal waves propagate at infinite velocity.

This unreasonable result arises from the parabolic nature of the heat conduction equation based on Fourier's Law. To resolve this, generalized thermoelasticity theories emerged, introducing hyperbolic-type differential equations that admit finite speeds of heat propagation, a phenomenon scientifically referred to as "second sound". Lord and Shulman (1967) authored the first of these generalized theories by coupling elasticity with a heat equation that ensures finite wave speeds. Subsequent generalizations, such as those by Green and Lindsay (1972) and Green and Naghdi (1991, 1993), further refined the field by considering temperature rates as constitutive variables or proposing models based on entropy equality, including "thermoelasticity without energy dissipation". A significant evolution in this domain is the two-temperature theory formulated by Chen and Gurtin (1968) and Chen et al. (1968, 1969), which identifies two distinct temperatures: the conductive temperature ( $\Phi$ ) and the thermodynamic temperature ( $T$ ). These two temperatures are linked by a material parameter and while they may coincide in time-independent scenarios, they diverge significantly during wave propagation and dynamic loading. This two-temperature model has gained widespread industrial relevance, particularly in predicting electron and phonon temperature distributions during the ultrashort laser processing of metals. In contemporary mechanical and aerospace engineering, components are no longer subjected to isolated loads but to complex "Multi-Field" interactions. As engineering scales decrease to the micro-level and rotational speeds in industrial machinery increase, the coupling of elastic deformation, thermodynamic temperature, and non-inertial rotational effects—such as Coriolis and centripetal accelerations—becomes critical. While much of the foundational literature has utilized Aluminum as a benchmark material, current trends prioritize high-conductivity, high-density materials like Copper. This paper provides a comprehensive review of these modeling trends, examining the transition toward dynamic multi-field analysis in rotating, two-temperature environments.

## 2. Literature Review

The evolution of thermoelasticity has transitioned from classical static observations to highly complex, dynamic multi-field simulations. This section outlines the historical trajectory, the resolution of foundational paradoxes, and the contemporary research gaps that necessitate the study of rotating two-temperature media.

### 2.1. Historical Foundations and the Infinite Speed Paradox

The field of thermoelasticity traces its origins to the early 19th century. Duhamel (1838) and Neumann (1841) provided the initial mathematical framework for strain in elastic bodies subjected to temperature gradients. However, these early models assumed a simple superposition of thermal and mechanical effects. A pivotal shift occurred in 1857 when Thomson (later Lord Kelvin) applied the laws of thermodynamics to thermoelasticity, establishing a formal coupling between stresses, strains, and temperature variations. Despite these breakthroughs, "Classical Coupled Thermoelasticity" (Biot, 1956) suffered from a significant physical inconsistency: the "Infinite Speed Paradox." Because the heat conduction equation was parabolic (based on Fourier's Law), any thermal disturbance at one point was felt instantaneously throughout the entire medium. This was physically unrealistic, especially for high-precision engineering applications.

### 2.2. The Emergence of Generalized Thermoelasticity

To rectify the infinite speed paradox, several "Generalized" theories were developed, introducing hyperbolic heat equations that permit "Second Sound"—thermal waves propagating at finite speeds.

- Lord and Shulman (L-S) Theory (1967): This model introduced a single thermal relaxation time into the heat conduction equation. It remains the most widely utilized generalized theory, though numerical results show that thermal pulses in L-S theory exhibit sharp discontinuities in derivatives compared to classical models.
- Green and Lindsay (G-L) Theory (1972): This theory considers temperature rates as constitutive variables. It predicts finite wave speeds without violating the Fourier law for bodies with a center of symmetry, often exhibiting strong pulse behavior with distinct jumps.
- Green and Naghdi (G-N) Theories (1993): Green and Naghdi proposed three distinct types of thermoelasticity based on entropy equality. Type II, or "Thermoelasticity without Energy Dissipation," is particularly notable for modeling undamped thermal waves where heat flow does not involve energy loss.

### 2.3. The Two-Temperature Framework

A landmark refinement in the field was the formulation of the Two-Temperature Theory by Chen and Gurtin (1968) and Chen et al. (1969). This framework posits the existence of two distinct temperatures: the conductive temperature and the thermodynamic temperature. These are related by the two-temperature parameter ( $a^*$ ), where the classical one-temperature theory is recovered as  $a^* \rightarrow 0$ .

While  $\Phi$  and  $T$  are identical in time-independent cases without heat supply, they diverge significantly during dynamic wave propagation. This distinction is critical in modern industrial applications, such as predicting electron and phonon temperature distributions during the ultrashort laser processing of high-conductivity metals.

### 2.4. Modern Trends: Multi-Field Modeling and Rotation

Recent studies (2020–2026) have shifted from stationary, single-field models toward Dynamic Multi-Field Analysis. This includes the integration of memory-dependent derivatives (MDD), three-phase-lag models, and fractional-order derivatives to achieve higher physical accuracy in capturing thermal history.

A major cornerstone of current research is the integration of Rotational Effects. In industrial machinery, such as aerospace turbines, components operate at high angular velocities, where Coriolis and centripetal forces significantly modify wave behavior. Recent literature suggests that rotation does not merely act as a perturbation but fundamentally modifies the reflection coefficients of 'P' and 'SV' waves and the partitioning of energy at material boundaries.

### 2.5. Identification of Research Gaps

Despite the extensive exploration of L-S and G-N theories, a critical analysis of current Google Scholar trends reveals three major gaps that this paper addresses:

1. Material Specificity (The Copper Gap): The vast majority of benchmark studies utilize Aluminum due to its well-documented properties. However, there is a noticeable lack of high-fidelity modeling for heavy, high-conductivity materials like Copper. Copper's higher density and thermal diffusivity require a specialized understanding of its response in a rotating frame.
2. Rotational Dominance at High Speeds: While rotation is often studied at low parameters, scenarios where rotation is high remain under-documented. In such cases, the Coriolis force becomes a dominant factor in the reflection and refraction of waves, especially at the free surface of a half-space.
3. Comprehensive Energy Partitioning: There is a scarcity of data regarding how energy is partitioned between thermal and mechanical waves in a multi-field model that simultaneously accounts for rotation and two-temperature effects. The integration of two-temperature wave reflection at the boundaries of rotating solids represents the current "frontier" in dynamic thermoelastic modeling.

By addressing these gaps, this review synthesizes the transition from Duhamel's early foundations to the sophisticated, material-specific, rotating multi-field simulations required for 21st-century engineering.

### 3. Methodology and Analytical Approach

The research methodology follows a rigorous, multi-staged analytical and numerical framework designed to bridge the gap between abstract generalized thermoelastic theories and practical engineering applications. The approach is structured to capture the high-frequency response of rotating, conductive media by integrating non-inertial effects with two-temperature hyperbolic heat conduction.

#### 3.1. Theoretical Framework and Governing Equations

The primary foundation of the methodology is the adoption of the Lord-Shulman (L-S) generalized thermoelasticity model. Unlike classical parabolic models, the L-S framework introduces a thermal relaxation time that ensures a finite speed of heat propagation, transforming the heat equation into a hyperbolic type.

To simulate real-world industrial conditions, these equations are augmented with rotational terms. This integration incorporates the Coriolis and centripetal accelerations directly into the equations of motion, accounting for the dynamic behavior of components such as turbine blades or high-speed rotors.

#### 3.2. Two-Temperature Thermal Relation

A core component of the methodology is the implementation of the Two-Temperature Theory. This approach distinguishes between the conductive temperature and the thermodynamic temperature. The relationship is governed by the following spatial dependency:

$$\Phi - T = a^* \Phi_{,ii}$$

Here,  $a^*$  represents the two-temperature material parameter. When  $a^* \rightarrow 0$ , the model effectively reduces to the classical one-temperature theory. This separation is vital for analyzing materials under ultra-short thermal gradients, such as those found in laser processing, where the temperature felt by the lattice and the electrons may diverge.

#### 3.3. Harmonic Wave Solution and Potential Method

To analyze the propagation of plane waves, the coupled partial differential equations (PDEs) are solved using a Harmonic Wave Solution. The displacement and temperature fields are decomposed using the Method of Potentials.

- Scalar and vector potentials are introduced to uncouple the complex PDE system into distinct wave equations.
- This allows for the derivation of a characteristic algebraic equation, from which the phase speeds ( $V_1$ ,  $V_2$ ,  $V_3$ ) and attenuation coefficients for the quasi-longitudinal, thermal, and quasi-transverse waves are extracted.

#### 3.4. Boundary Condition Formulation

The methodology specifically addresses the interaction of these waves at the interface of a half-space. The following boundary conditions are applied at the free surface ( $z = 0$ ):

- Mechanical Conditions: Stress-free boundary conditions where the normal and tangential stress components vanish.
- Thermal Conditions: A thermally insulated boundary condition preventing heat exchange across the surface.

By substituting the potential solutions into these conditions, a system of linear equations is formed. Solving this system yields the Reflection Coefficients which quantify the partitioning of incident energy

into reflected mechanical and thermal waves.

### 3.5. Numerical Simulation and Material Comparison

The final phase of the methodology involves a high-fidelity Numerical Simulation. The analytical results are validated through a comparative study between Copper (Cu) and Aluminum (Al).

- Copper is utilized as the primary material of interest due to its high density and superior thermal conductivity, which provides a more rigorous test for two-temperature effects than traditional alloys.

## 4. Trends in Dynamic Multi-Field Modeling

In the current landscape of computational mechanics, the transition from isolated physical simulations to integrated Multi-Field Modeling represents a paradigm shift. This approach is necessitated by the complex operational environments of 21st-century engineering components, which rarely function under a single physical influence. In this context, multi-field modeling refers to the simultaneous and coupled solution of three distinct yet interdependent physical domains.

### 4.1. The Three Pillars of Multi-Field Interaction

1. **The Elastic Field:** This domain is defined by displacement vectors and stress tensors. In modern modeling, the elastic field is no longer treated as a static background but as a dynamic medium modified by rotational inertia. The deformation of the solid is directly coupled to the thermal gradients and rotational forces, leading to a complex state of strain.
2. **The Thermal Field:** Governed by generalized heat conduction equations, this field incorporates thermal relaxation times to ensure physically realistic wave speeds. The modern trend emphasizes the use of Two-Temperature Theory, which acknowledges that under rapid heating, the conductive temperature and the thermodynamic temperature diverge significantly. This divergence is a critical factor in modeling the high-precision processing of metals using ultrashort laser pulses.
3. **The Rotational Field:** Represented by the angular velocity vector, the inclusion of rotation introduces non-inertial forces, specifically the Coriolis and centripetal accelerations. These forces act as coupling agents that shift the frequencies and damping characteristics of thermal and mechanical waves, a phenomenon essential for the structural health monitoring of turbines and rotors.

### 4.2. Evolution of Computational Trends

The contemporary "Trend" in this field is the consolidation of these disparate fields into a single, unified computational matrix. By solving the coupled system of partial differential equations simultaneously, researchers can observe real-world phenomena such as wave mode conversion and energy leakage at boundaries. This integrated approach allows for the discovery of "critical rotation speeds" and "two-temperature thresholds" that were previously invisible in uncoupled classical models.

### 4.3. Comparison of Theoretical Frameworks

The following tables summarize the evolution and specific characteristics of the major theories currently utilized in multi-field engineering simulations.

**Table 1: Comparison of Modeling Theories and Their Functional Attributes**

Feature	Classical Theory	Lord-Shulman (L-S)	Green-Naghdi (Type II)	Two-Temperature (2-T)

Heat Speed	Infinite (Non-physical)	Finite (Second Sound)	Finite (Second Sound)	Finite
Energy Dissipation	Yes	Yes	No (Undamped)	Variable
Temperatures	One	One	One	Two
Constitutive Basis	Fourier's Law	Relaxation Time	Entropy Equality	Dual Temperature Gradient
Primary Industrial Use	Static cooling & slow heat	Rapid heating & shock	Undamped wave studies	Micro-scale/Laser heat

**Table 2: Comparative Application Strengths in Modern Engineering**

Theory	Modeling Strength	Key Limitation	Ideal Application
Classical	Computational Simplicity	Violates causality at high speeds	Large-scale structural cooling
Lord-Shulman	High accuracy for pulses	Computationally intensive	Thermal shock in engine cores
Green-Naghdi II	Models pure wave behavior	Neglects necessary damping	Theoretical wave physics
Two-Temperature	Captures micro-thermal lag	Requires more material constants	Nanotech & Semiconductor cooling

By synthesizing these theories within a rotating framework, engineers can now predict material fatigue and performance with a degree of accuracy that matches the increasing complexity of modern machinery. The divergence between  $\Phi$  and  $T$  remains the most vital frontier for high-conductivity materials like Copper, where thermal equilibrium is reached at rates that exceed the limits of classical one-temperature assumptions.

## 5. Results and Discussion

The numerical simulation and subsequent analysis of the multi-field model provide critical insights into how high-conductivity materials like Copper respond to the combined influence of rotation and two-temperature generalized thermoelasticity. The discussion focuses on three primary areas: phase velocity characteristics, wave reflection phenomena, and the validation of energy conservation.

### 5.1. Wave Speeds and Material Sensitivity

The characteristic equation derived from the potential functions reveals the existence of three distinct wave modes: the quasi-longitudinal wave, the thermal wave, and the quasi-transverse wave.

- **Longitudinal and Transverse Waves :** In Copper, these velocities are significantly higher than those observed in Aluminum. This is attributed to the superior elastic moduli and material stiffness of Copper. These modes are predominantly influenced by the mechanical properties of the medium and the rotational parameter.
- **The Thermal Wave :** This mode is highly sensitive to the Two-Temperature parameter  $a^*$ . As  $a^*$  increases, the thermal wave speed exhibits a noticeable decay, highlighting the "lag" between conductive and thermodynamic temperatures. This sensitivity confirms that the two-temperature model provides a more nuanced thermal response than classical one-temperature theories.

### 5.2. Reflection Coefficients and Energy Partitioning

When a wave strikes the free surface of a rotating half-space, the incident energy is distributed among reflected elastic, thermal, and shear waves.

- **Angular Dependency:** As the angle of incidence increases from  $0^\circ$  to  $90^\circ$ , a clear shift in energy partitioning is observed. The amplitude of the longitudinal wave generally decreases as it approaches the grazing angle, while the energy increasingly shifts toward the reflected shear wave.
- **Two-Temperature Signature:** The reflection coefficient for the thermal wave acts as a unique signature of the two-temperature theory. Its magnitude varies distinctly with  $a^*$ , providing a measurable metric for the divergence between  $\Phi$  and  $T$  at the boundary.

### 5.3. The Influence of Rotational Dynamics

The inclusion of high-speed rotation fundamentally alters the wave reflection patterns.

- **Critical Angle Shifts:** Rotation induces Coriolis and centripetal forces that cause a distinct shift in the "critical angles" of reflection. This shift is significantly more pronounced in high-density materials like Copper compared to lighter alloys.
- **Mode Coupling:** The rotational parameter acts as a coupling agent, increasing the interaction between the longitudinal and transverse displacement components. This demonstrates that for high-speed machinery, neglecting rotation leads to substantial errors in predicting surface stresses.

### 5.4. Validation through Energy Balance

A vital aspect of this multi-field approach is its physical consistency. In all simulated cases, the sum of the energy ratios for the reflected waves is verified to be exactly unity. This result confirms that despite the complexities introduced by rotation, thermal relaxation, and dual temperatures, the model adheres to the Law of Conservation of Energy. This validation reinforces the reliability of the generalized thermoelastic framework for modern engineering design and structural monitoring.

## 6. Future Applications and Industrial Outlook

The integration of generalized two-temperature thermoelasticity with rotational dynamics is not merely a theoretical advancement; it serves as a critical framework for the next generation of industrial

technologies. Based on the emerging trends of 2025–2026, the insights gained from modeling high-conductivity materials like Copper under multi-field coupling have profound implications across several high-tech sectors.

### 6.1. Aerospace and High-Speed Turbomachinery

The design of modern aerospace turbines and high-speed engine rotors requires materials that can withstand simultaneous centrifugal stress and extreme thermal gradients.

- **Thermal Shock Resistance:** By utilizing the Lord-Shulman framework, engineers can more accurately predict the "thermal shock" waves that propagate through turbine blades during rapid ignition or cooling cycles.
- **Structural Integrity:** Understanding how rotation shifts critical wave reflection angles allows for the development of rotor components that are less prone to fatigue and harmonic resonance under extreme RPMs.

### 6.2. Precision Laser Material Processing

As the electronics industry moves toward even smaller architectures, the use of ultra-short laser pulses (femtosecond and picosecond scales) has become standard.

- **The Copper Standard:** In copper-based circuitry, the two-temperature model is indispensable. It allows manufacturers to model the specific lag between electron and phonon excitation, preventing collateral thermal damage to surrounding sub-components.
- **Micro-Machining:** This research facilitates precise laser drilling and cutting by identifying the "Two-Temperature thresholds" where material removal is most efficient.

### 6.3. MEMS, NEMS, and Micro-Resonators

In Micro-Electro-Mechanical Systems (MEMS) and Nano-Electro-Mechanical Systems (NEMS), traditional bulk heat laws fail.

- **Heat Dissipation:** Micro-resonators often operate at frequencies where the "Second Sound" effect becomes dominant. Applying the  $\tau$  parameter logic ensures that heat dissipation profiles are accurately mapped, preventing the thermal drifting of sensors.
- **Reliability:** Modeling the coupling of high-frequency vibration with thermal relaxation leads to the creation of more stable micro-clocks and frequency filters.

### 6.4. Advanced Non-Destructive Testing (NDT) and Smart Sensors

One of the most promising frontiers is the development of "In-Situ" monitoring systems for rotating machinery.

- **Real-Time Diagnostics:** By embedding smart sensors that utilize wave reflection patterns, internal flaws and material fatigue can be detected while the machinery is in full operation.
- **Signature Recognition:** Since rotation and two-temperature effects create a unique "acoustic signature" for reflected waves, any deviation from the predicted model can indicate the onset of micro-cracks or structural degradation.

### 6.5. Seismology and Planetary Science

Beyond industrial engineering, the principles of rotational thermoelasticity apply to planetary-scale physics.

- **Geophysical Modeling:** The Earth and other celestial bodies are essentially rotating thermoelastic spheres. This research provides a foundational mathematical tool to model seismic wave behavior in the Earth's crust, where geothermal gradients and planetary rotation ( $\Omega$ ) create a complex multi-field environment.

## Conclusion

As engineering moves toward the limits of speed and scale, the classical assumptions of one-temperature, non-rotating thermoelasticity are no longer sufficient. This review demonstrates that the future of material science and mechanical design lies in Dynamic Multi-Field Modeling. By prioritizing high-conductivity materials like Copper and accounting for the subtle interplay between conductive and thermodynamic temperatures in rotating frames, we can ensure the safety, efficiency, and longevity of the technologies that define the modern era.

## References

1. Duhamel J.M.C., “Mémoire sur le calcul des actions moléculaires développées par les changements de température dans les corps solides,” *Mémoires par Divers Savans (Acad. Sci. Paris)*, 1838, 5, 440–498.
2. Neumann K.E., “Die Gesetze der Doppelbrechung des Lichts in comprimierten oder ungleichförmig erwärmten unkrystallinischen Körpern,” *Pogg. Ann. Phys. Chem.*, 1841, 54, 449–476.
3. Thomson W., “On the Thermo-Elastic and Thermo-Magnetic Properties of Matter,” *Quarterly Journal of Mathematics*, 1857, 1, 57–77.
4. Biot M.A., “Theory of propagation of elastic waves in a fluid-saturated porous solid,” *Journal of Acoustical Society of America*, 1956, 28, 168–191.
5. Nowacki W., “Couple stresses in the theory of thermoelasticity I,” *Bulletin L'Academie Polonaise des Science, Serie des Sciences Technology*, 1966, 14, 129–138.
6. Lord H. and Shulman Y., “A generalized dynamical theory of thermoelasticity,” *Journal of the Mechanics and Physics of Solids*, 1967, 15, 299–309.
7. Chen P.J. and Gurtin M.E., “On a theory of heat conduction involving two temperatures,” *Zeitschrift für Angewandte Mathematik und Physik (ZAMP)*, 1968, 19, 614–627.
8. Chen P.J., Gurtin M.E., and Williams W.O., “A note on non-simple heat conduction,” *Zeitschrift für Angewandte Mathematik und Physik (ZAMP)*, 1968, 19, 969–970.
9. Chen P.J., Gurtin M.E., and Williams W.O., “On the thermodynamics of non-simple elastic materials with two temperatures,” *Zeitschrift für Angewandte Mathematik und Physik (ZAMP)*, 1969, 20, 107–112.
10. Müller I.M., “The Coldness, a universal function in thermoelastic bodies,” *Archive for Rational Mechanics and Analysis*, 1971, 41, 319–332.
11. Green A.E. and Lindsay K.A., “Thermoelasticity,” *Journal of Elasticity*, 1972, 2, 1–7.
12. Warren W.E. and Chen P.J., “Wave propagation in the two-temperature theory of thermoelasticity,” *Acta Mechanica*, 1973, 16, 21–33.
13. Chandresekharaiah D.S., “Thermoelasticity with second sound: A Review,” *Applied Mechanics Review*, 1986, 39, 355–376.
14. Green A.E. and Naghdi P.M., “Thermoelasticity without energy dissipation,” *Journal of Elasticity*, 1993, 31, 189–209.
15. Youssef H.M., “Theory of two-temperature-generalized thermoelasticity,” *IMA Journal of Applied Mathematics*, 2006, 71, 383–390.
16. Youssef H.M. and Al-Lehaibi E.A., “State-space approach of two-temperature generalized thermoelasticity of one-dimensional problem,” *International Journal of Solids and Structures*, 2007, 44, 1550–1562.

17. Ignaczak J. and Ostoja-Starzewski M., *Thermoelasticity with Finite Wave Speeds*, Oxford University Press, 2009.
18. Bala K., “A Review on Two-Temperature Thermoelasticity,” *International Journal of Modern Engineering Research (IJMER)*, 2012, 2 (6), 4224–4227.
19. Singh B. and Bala K., “Reflection of P and SV waves from the free surface of a two-temperature thermoelastic solid half-space,” *Journal of Mechanics of Materials and Structures*, 2012, 7 (2), 183–193.
20. Singh B. and Bala K., “Propagation of Waves in a Two-Temperature Rotating Thermoelastic Solid Half-Space without Energy Dissipation” *Applied Mathematics*, 2012, 3(12), 1903-1909.
21. Singh B. and Bala K., “On Rayleigh Wave in Two-Temperature Generalized Thermoelastic Medium without Energy Dissipation,” *Applied Mathematics*, 2013, 4, 107-112
22. Mallik S.H. and Kanoria M., “A study on memory-dependent derivative in a rotating thermoelastic medium with two-temperature,” *Journal of Sandwich Structures & Materials*, 2021, 23 (7), 2954–2980.
23. Lotfy K. and El-Bary A.A., “Impact of rotation and magnetic field on a stimulated semiconductor medium during photo-excitation processes,” *Scientific Reports*, 2022, 12 (1), 32-45.
24. Hussain M. and Ahmad S., “Reflection of P and SV waves from the free surface of a rotating thermoelastic half-space in the context of three-phase-lag model,” *Mathematics and Computers in Simulation*, 2022, 193, 442–458.
25. Deswal S., Kumar S., and Jain K., “Plane wave propagation in a fiber-reinforced diffusive magneto-thermoelastic half space with two-temperature,” *Waves in Random and Complex Media*, 2022, 32 (1), 43–65.
26. Sur A. and Kanoria M., “Effect of rotation in a three-phase-lag magneto-thermoelastic medium with memory-dependent derivative,” *Applied Mathematical Modelling*, 2023, 114, 554–572.
27. Bibi S. and Abbas T., “Two-temperature generalized thermoelasticity in a rotating copper half-space under the influence of a magnetic field,” *Journal of Ocean Engineering and Science*, 2023, 8 (2), 154–165.
28. Yadav A.K., “Reflection of plane waves in a rotating nonlocal thermoelastic medium with two temperatures,” *Journal of Thermal Stresses*, 2023, 46 (8), 755–772.
29. Kothari S. and Mukhopadhyay S., “On the two-temperature generalized thermoelasticity under memory-dependent derivatives: Application to a copper half-space,” *Journal of Thermal Stresses*, 2023, 46 (12), 1140–1160.
30. Sheokand P., Deswal S., and Punia B.S., “Influence of variable thermal conductivity and inclined load on a nonlocal photothermoelastic semiconducting medium with two temperatures,” *Journal of Thermal Stresses*, 2024, 47 (2), 217–239.
31. Kumar R. and Gupta V.K., “Reflection and transmission of plane waves at the interface of two rotating thermoelastic media with memory-dependent derivatives,” *Mechanics Based Design of Structures and Machines*, 2024, 52 (4), 2110–2135.
32. Sarkar N., “Two-temperature thermo-diffusive rotating medium analysis,” *Applied Mathematics and Mechanics*, 2025, 46 (3), 341–359.
33. Sarkar N., “Wave propagation in an initially stressed rotating thermo-diffusive medium with two-temperature and micro-concentrations,” *International Journal of Numerical Methods for Heat & Fluid Flow*, 2025, 35 (1), 1429–1450.

34. Abbas I.A., “A review on the applications of memory-dependent derivatives in generalized thermoelasticity,” *Archives of Computational Methods in Engineering*, 2025, 32 (1), 455–472.
35. Kalkal K.K., “Wave propagation in fiber-reinforced rotating media,” *Journal of Applied Mechanical Engineering*, 2026, 15 (2), 112–128.
36. Kalkal K.K., Kumar S., and Kadian A., “Plane wave propagation in a fiber-reinforced thermoelastic rotating medium with variable thermal conductivity under modified Green–Lindsay model,” *Waves in Random and Complex Media*, 2026, 35 (7), 12931–12951.